

# **Review Article**

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# Choice of Rods in Surgical Treatment of Adolescent Idiopathic Scoliosis: What Are the Clinical Implications of Biomechanical Properties? – A Review of the Literature

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The surgical treatment of adolescent idiopathic scoliosis (AIS) involves 3-dimensional curve correction with multisegmental pedicle screws attached to contoured bilateral rods. The substantial corrective forces exert a high level of stress on the rods, and the ability of the rod to withstand these forces without undergoing permanent deformation relies on its biomechanical properties. These properties, in turn, are dependent on the material, diameter, and shape of the rod. The surgical treatment of AIS is characterized by the requirement for a special biomechanical profile that may differ substantially from what is needed for adult deformity surgery. This overview summarizes the current knowledge of rod biomechanics in frequently used rod constructs, with a particular focus on translational research between biomechanical studies and clinical applicability in AIS patients.

Keywords: Scoliosis, Surgery, Adolescent, Spinal fusion, Methods

## **INTRODUCTION**

Surgical treatment of adolescent idiopathic scoliosis (AIS) is complex and involves extensive 3-dimensional (3D) correction and fusion of the spine while avoiding intraoperative complications such as pedicle fractures, dural tears, excessive bleeding and neurological deterioration. Standard surgical treatment of AIS patients involves posterior multisegmental pedicle screw insertion in the length of the intended fusion. With pedicle screws connected to dual rods the deformity is corrected using one or multiple different techniques including translation, distraction-compression, rod derotation, direct vertebral derotation, cantilever, *in situ* bending or vertebral coplanar alignment.<sup>1-4</sup> Before insertion, the rods are bend to the desired sagittal contour to achieve a balanced spine with a natural lordosis/kyphosis profile (Fig. 1). The success of these intraoperative corrective

maneuvers is highly dependent on rod biomechanics as they exert high levels of stress on the rods. Corrective forces increase the risk of plastic deformation of the rod and subsequent loss of correction due to the low viscoelasticity of the tissue.<sup>5</sup> A thorough understanding of the stress and strains exerted on the rods due to contouring and the forces and torques applied during correction can ultimate improve clinical results in AIS surgery. Despite extensive research into the potential benefits and side effect of different rod constructs there is no universal agreement as to the optimal biomechanical properties.

AIS patients often present with a preoperative hypokyphosis and the restoration of sagittal alignment has received increasing attention in recent years. Several studies have shown that allpedicle screw constructs may be associated with a failure to restore thoracic kyphosis to a normal range postoperatively.<sup>6-8</sup> Postoperative hypokyphosis can lead to increased risk of adjacent



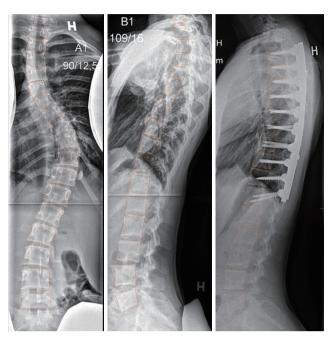
**Fig. 1.** Rod contouring using a French bender whereby a physiological sagittal profile is mimicked prior to rod insertion.

segment disease and poorer quality of life and should be a main concern during surgery. The lack of kyphosis restoration has been attributed to the corrective maneuvers but has also been associated with the biomechanical properties of the construct (Fig. 2). 16,17

The ultimate goal of AIS surgery is to correct the deformity, ensure a balanced spine with level shoulders, and prevent curve deterioration.<sup>18</sup> The current trend in AIS surgery is to use higher pedicle screw density to increase load sharing and apply stiffer rod constructs to avoid rod deformation and loss of correction in both the coronal, sagittal and axial plane. This development has been largely driven by biomechanical studies suggesting improved sustainability of the correction using this approach. However, increased construct stiffness may have side effects; as implant-bone fixation is increased, a higher proportional load is transferred to the rod, which decreases the physiological stress on the bone. This may impact bone quality long-term although no studies have verified this theory in AIS patients. Furthermore, increased rod stiffness may add to the junctional stress on the levels adjacent to the instrumentation which increase the risk of adjacent segment disease<sup>19</sup> or decompensation above the implant. The biomechanical profile of a rod largely depends on diameter, shape and material properties. This overview aims to describe these concepts and assess the potential advantages and pitfalls of their clinical use in surgical treatment of AIS.

#### **BIOMECHANICAL PROPERTIES**

Biomechanical properties of spinal rods are typically differentiated by yield strength and stiffness. The yield strength, or yield stress, can be defined as the stress at which permanent deformation occurs. Stiffness, or rigidity, can be defined as the extent to which a rod resists deformation in response to an applied



**Fig. 2.** A main thoracic curve with a preoperative severe hypokyphosis (lordosis). The lordosis is only minimally improved after surgery and a proximal junctional kyphosis is developing.

force. This is often reported as Young's modulus, which is measure of material elasticity (or stiffness) and is also known as the elastic modulus. The difference between yield strength and stiffness can be exemplified by a classic rubber band that requires very little stress to deform (low stiffness) but a much higher stress is needed for permanent deformation (high yield strength). While these material properties can be easily measured in a laboratory setting the theoretical implications cannot necessarily be transferred to the clinical reality. Furthermore, Ayers et al.<sup>20</sup> found that the biomechanical profile of a given rod was very sensitive to differences in production as individual properties varied greatly between manufacturers for the same material. Pienkowski et al.<sup>21</sup> showed that fatigue life of the implant was explained by implant type rather than material further adding to the complexity of understanding rod biomechanics.

#### **ROD MATERIAL**

The most frequently reported rod materials used in AIS corrective surgery are stainless steel (SS) or ultrahigh strength stainless steel (UHSS), titanium alloy (Ti), and cobalt chromium (CoCr) (Table 1). $^{22}$ 

Generally, Ti is characterized by high yield strength but a lower stiffness compared to SS, UHSS and CoCr. CoCr has only in recent years been introduced in AIS surgery but is character-

**Table 1.** Mechanical properties of 3 main groups of spinal implants in adolescent idiopathic scoliosis surgery<sup>22</sup>

Biomaterial	Elastic modulus (Young's modu- lus) (Gpa)	Yield strength (MPa)	Fatigue strength (MPa)
CoCr alloys	200-300	300-2,000	207-950
Titanium alloys	110-116	485-1,034	300-389
Stainless steel	190	792	241-820

CoCr, cobalt chromium.

ized by a very high stiffness and low yield strength. <sup>23,24</sup> Ti originally gained popularity in both adult and adolescent spine deformity surgery due to a high biocompatibility, corrosion resistance and magnetic resonance imaging (MRI) compatibility. Scuderi et al. <sup>25</sup> examined the presence of MRI artifacts in an animal model between Ti, SS, and CoCr. Ti rods showed the least amount of artefacts followed by CoCr while SS showed the highest amount. Several studies have verified these finding although Trammell et al. <sup>26</sup> and Ahmad et al. <sup>27</sup> found that the difference in artefacts between Ti and CoCr did not interfere with the evaluation of the spinal canal and surrounding neural elements. It has been reported that Ti compared to SS produce substantially better overall diagnostic quality <sup>28-30</sup> although the clinical implication of this difference has not been established.

Serhan et al.<sup>31</sup> conducted a biomechanical study comparing Ti, CoCr, UHSS, and SS. Rods were contoured with one-plane bending and placed in a synthetic spine model imitating spinal deformity correction. After removal from the construct 90% of Ti rod retained their original shape versus 77%, 63%, and 54% of UHSS, SS and CoCr, respectively, illustrating the lower yield strength of the latter materials. Conversely, when the corrective forces were measured in-construct, UHSS and CoCr were found to have 42% higher corrective forces compared to Ti due to a higher stiffness.

AIS surgery involves rod contouring to mimic the sagittal profile with a lumbar lordosis followed by a thoracic kyphosis within the normal range (Fig. 1). This intraoperative bending of the rod introduces cracks or dents in the material, which can reduce the endurance limit of the rod, also termed the "notch effect". Slivka et al.<sup>32</sup> found that the endurance limit of CoCr was at least 25% higher than UHSS, SS, or TI in response to repetitive bending whereas Noshchenko et al.<sup>33</sup> showed the highest "springback" (or yield strength) in Ti rods compared to SS. Wedemeyer et al.<sup>34</sup> in a bovine model, confirmed that Tis can withstand higher strains and yield than the relatively brittle SS before failure occurs after bending. However, Lindsey et al.<sup>35</sup>

contradicted these results demonstrating a lower fatigue life of Ti compared to SS in response to bending. Burger et al.<sup>36</sup> performed 3-point bending on Ti and SS rods and stored the rods for 8 months at 37°C temperature to mimic a physiological environment. Ti rods lost correction corresponding to 6° per year for a 300-mm rod, which was considerably more than SS rods.

A few clinical studies have investigated the importance of rod material in AIS patients. Lamerain et al.<sup>37</sup> compared SS with CoCr rods in 90 AIS patients and found significantly better coronal curve correction, reduced loss of correction and a better kyphosis restoration using CoCr rods. Angelliaume et al.<sup>38</sup> using hybrid constructs found that coronal curve correction was similar for Ti and CoCr constructs but that a better kyphosis restoration was seen in the CoCr group. Cidambi et al.<sup>39</sup> using 5.5-mm UHSS found that the rod on the concave side of the curve flattened by 21° 4–6 weeks postoperatively, which was similar to the results from Salmingo et al.<sup>40</sup> showing 16° deformation of Ti rods. Le Navéaux et al.<sup>41</sup> showed that even in stiff 5.5-mm CoCr constructs some postoperative 3D rod deformation can be expected.

#### ROD DIAMETER AND PROFILE

Surgeons may choose rods of different diameters to achieve the desired biomechanics in any given case. An increase in radius alters stiffness to the 4th power of the change in radius. Consequently, the bending stiffness increases from 5.17 EI (Nm²) for a rod diameter of 5.5 to 9.18 EI (Nm²) for a rod diameter of 6.35 mm. A change in rod diameter is therefore bound to result in a stiffer construct but whether this is beneficial to AIS patients is a crucial point of interest.

Huang et al.<sup>42</sup> compared 5.5-mm vs. 6.35-mm Ti rods in 93 AIS patient and found no difference in curve correction, loss of correction or coronal global balance. Liu et al.<sup>43</sup> also reported similar coronal curve correction of single thoracic curves, however the authors found a significantly better kyphosis restoration with the 6.35-mm rods. Abul-Kasim<sup>44</sup> made a similar observation in 116 AIS patients reporting a better kyphosis restoration and derotation with higher diameter rods but with no difference in coronal correction. Fletcher et al.<sup>45</sup> reported 2-year follow-up on 214 AIS patients and found that 72% vs. 47% had a normal kyphosis in the 6.35 and 5.5 mm groups, respectively. In contrast to these studies Prince et al reported on a national database of 163 pediatric scoliosis patients and found the 5.5 mm group to have a significantly better curve correction 2 years postoperatively compared to 6.35-mm rods. Rod diameter was

not found to be predictive of sagittal plane correction. The analysis, however, did not adjust for rod material and the cohort included non-AIS patients.

In recent years, a few studies have examined the potential benefits of using a noncircular rod. In a biomechanical simulation Cui et al.<sup>46</sup> found that for a given cross-sectional area, the axial stiffness rises by about 2.5% and the maximum stress drops by up to 22% when the section is square compared to when it is circular. Gehrchen et al.<sup>16</sup> reported the immediate curve correction comparing circular and "beam-like" rods in 129 AIS patients. Coronal curve correction was found to be 9% higher in the beam-like group. A failure to restore thoracic kyphosis was seen but with no significant difference between the 2 groups.

#### HYBRID RODS OR CONSTRUCTS

Proximal junctional kyphosis (PJK) is an abnormal kyphosis that develops at the upper instrumented vertebra in response to fusion. It is a relatively common finding after AIS deformity surgery and is universally considered a unsatisfactory outcome. 47-49 Multiple factors have been associated with PJK including disruption of posterior ligaments and poor postoperative sagittal alignment or the use of all-pedicle screw constructs. It has also been suggested that a high construct rigidity can lead to increased junctional stress at the adjacent upper segment leading to forward decompensation and ultimately PJK. Han et al. 50 found that increasing the rigidity of the construct using multiple-rod CoCr vs. 2-rod Ti significantly increased the rate of PJK. In a subsequent study, Han et al.51 found that patients operated with CoCr rods compared to Ti more frequently developed PJK. It should be noted that these studies were conducted on adult deformity patients who differ in a number of ways from AIS patients.

Whether a gradual stress reduction at the proximal level of the construct could reduce the rate of PJK has been the focus of several studies. Lange et al.<sup>52</sup> investigated the effect of using cerclage wires at the proximal segment of a short lumbar fusion. At the proximal transition segment rigidity was reduced by about 60% compared to an all-pedicle screw construct. Facchinello et al.<sup>53</sup> and Thawrani et al.<sup>54</sup> reported similar results using proximal hooks showing lower stiffness at the upper instrumented level which applied less force on the anchors. Cahill et al.<sup>55</sup> using computer simulation showed that the use of a transition rod with a proximal decrease in diameter leads to less disc angulation compared to a standard construct. Maximum implant stress was theoretically reduced by up to 60%. This concept was ap-

plied in a clinical setting by Ohrt-Nissen et al.<sup>56</sup> who showed that the use of double transition rods in AIS corrective surgery resulted in an improved kyphosis restoration compared to a standard construct. However, whether this new rod concept can reduce the rate of PJK is not yet known.

#### SHAPE-MEMORY METAL RODS

Some authors have argued that the stiffness of the implant is not of clinical relevance as most available implant has a stiffness that far exceeds the need for stabile fusion. Some have advocated for the use of dynamic flexible rods to avoid predisposing the patients to PJK and adjacent disc degeneration by reducing the peak stress on the screw anchors during correction. 19,57 The shape-memory metal (SMM) Nitinol (a nickel-Ti) is characterized by an ability to recover from considerable deformation and return to a preconditioned shape when heated above its transformation temperature<sup>58,59</sup> (e.g., body temperature). This may be beneficial because the recovery properties of the rod apply a progressive and constant correction force, which would more gradually counteract the low viscoelasticity of the tissue that is responsible for rod flattening. A few clinical studies have described the use of SMM rods in scoliosis surgery. Wang et al.<sup>60,61</sup> showed satisfactory results using a SMM rod as a temporary rod during surgery to correct the deformity before replacing it with a rigid rod. A recent controlled randomized clinical pilot trial described the use of SMM rods as definitive treatment in AIS patients.<sup>62</sup> The authors found no difference in coronal or sagittal parameters compared to standard rods at 5-year followup and concluded that the SMM rods were safe and efficient for AIS corrective surgery.

#### **DISCUSSION**

The final outcome of AIS surgery relies not only on choice of rods but also patient characteristics (e.g., skeletal maturity, body mass index), curve type and surgical strategy. Surgical treatment of AIS is substantially different from adult deformity surgery and as such the desirable biomechanical properties of the rods are different. The literature is abundant with biomechanical studies on various implant types but there is a lack of high-quality clinical studies in AIS patients comparing implants. AIS corrective surgery is characterized by a high fusion rate compared to adult deformity patients and revision surgery is a rare event. As such, long-term durability of a rod material may have limited clinical applicability. While the higher yield strength of Ti

theoretically reduces the risk of rod fracture this complication is almost nonexistent in AIS patients and should not be a main priority in choice of rod. Huang et al.<sup>42</sup> discussed the theoretical disadvantage of using high-stiffness rods when considering the 20–30 fold lower Young Modulus of bone. This mismatch could decrease the stress on the bone-implant interface (stress shielding), which can lead to bone resorption and poor osteointegration. While this theory may apply in an elderly population it has not been shown to have any clinical relevance in AIS surgery.

It seems that the primary objectives of curve correction and sagittal restoration would be best achieved using a stiffer construct, which is minimally weakened by intraoperative contouring. This is likely the reason for the increasing popularity of CoCr and higher-diameter rods. However, high-quality studies on this topic are needed for any firm conclusions to be drawn. Furthermore, we encourage future studies to assess the efficacy of individually tailored rod that are bend at the manufacturing stage to minimize rod weakening during intraoperative contouring.

#### **CONCLUSION**

Clinical studies comparing biomechanical differences between rod constructs are generally of poor methodological quality with a high risk of bias. While curve correction does not seem to be substantially different between rod types there is some evidence to suggest that the sagittal profile may be more efficiently restored using stiffer rod constructs. The use of transition rods or shape memory rods may decrease junctional stress but the clinical applicability of these newer designs has not yet been firmly established.

## **CONFLICT OF INTEREST**

SO, MG, and BD received an institutional research grant from K2M outside the submitted work. MG and BD received an institutional research grant from Medtronic outside the submitted work

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